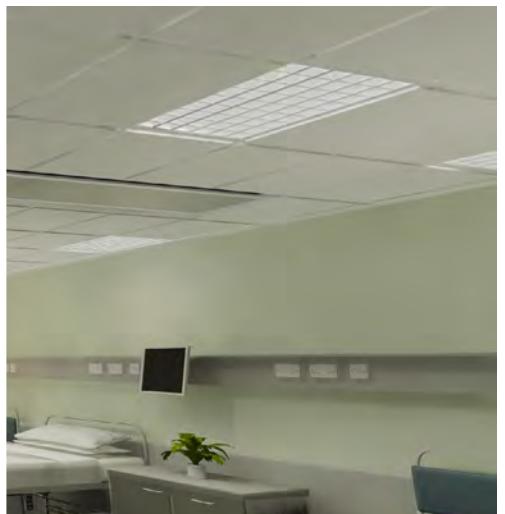


*the future of space conditioning*

## Eco-Healthcare HQ™

### active chilled beam





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# Product Description

Eco-Healthcare HQ is one of Frenger's latest range of high performance Chilled Beams. Energy efficiency has been a key driver for such advancements in Frenger's Chilled Beam Technology.

**Eco-Healthcare HQ is 230mm deep as standard** and can be increased to **270mm for higher air volumes**.

Eco-Healthcare HQ can achieve **1121 watts per meter total cooling** (based on  $10\Delta t_k$  and 25 ltrs/sec/m for a beam supplied at  $16^\circ C$  with a 100Pa).

The Eco-Healthcare HQ is constructed from "High Quality" extruded aluminium side profiles, powdercoat finish to all visible components that not only makes for a robust product that has precision interfaces, but also enhances performance. This beam also contains a number of **Frenger's Patent pending performance enhancing features** and as can be expected from the Frenger brand, the Eco-Healthcare HQ beam is also designed to be easily tailored to suit the unique parameters of individual project sites, for the optimum product / system efficiencies. This is partly achieved by Frenger's "burst nozzle" arrangement that not only encourages induction, but also reduces noise. Given the size and amount of burst nozzles being appropriately quantified for each project, this provides consistent jet velocities, equal distribution of the air discharge and continuous induction through the entire length of the heat exchanger (battery). There are no dead spots due to plugging back nozzles in the system to suit the amount of open standard nozzles sizes as associated with many competitors' active beams as dead spots and / or reduced jet velocities decrease their cooling capacities / efficiencies.

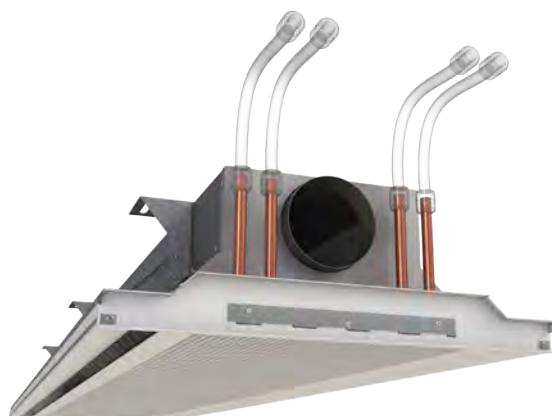
Frenger's heat exchanger batteries are also fitted with extruded aluminium profiles to not only enhance performance but also provide a continuous clip on facility for the underplate. This arrangement keeps the underplates true and flat for long lengths, even up to 3.6m.

Eco-Healthcare HQ is designed with hospital / healthcare environments in mind. The fin coil battery element can easily be lowered to allow cleaning of all four sides. Eco-Healthcare HQ units are "**powdercoat**" finished in RAL 9010 (20% Gloss) White as standard

Eco-Healthcare HQ is available in any length from 1.2m up to 3.6m in 0.1m increments and is constructed from a combination of zinc coated mild steel for non critical components, extruded aluminium where precision and a high quality robust construction is required.

The air chamber for Eco-Healthcare HQ is the largest in Frenger's product range and can accommodate up to 90 ltrs/sec with its 160mm diameter single air inlet connection point.

Eco-Healthcare HQ beams have a "closed back", thus meaning that all induced air (recirculated room air) is induced through the underplate within the room space to avoid any need for perimeter flash gaps and / or openings in the ceiling system. This also provides for a better quality of recirculated air as the recirculated air does not mix with any air from the ceiling void. The induction ratio of Eco-Healthcare HQ is typically 5 times that of the supply air (fresh air) rate.



In addition to Eco-Healthcare HQ's high cooling performance capability of in excess of 1000 watts per meter, **Eco-Healthcare HQ can operate well and induce at low air volumes, as little as 3 l/s/m and even with a low static pressure of just 40Pa**. Likewise **Eco-Healthcare HQ can handle high air volumes up to 30 l/s/m and up to 120Pa**. Please note however that there high air volumes should be avoided wherever possible and are the absolute maximum and should not ever be exceeded. As a "rule of thumb" 25 ltrs/sec/m from a 2 way discharge beam is the maximum for occupancy comfort compliance to BS EN 7730.

Eco-Healthcare HQ can have integrated heating with separate connections (2 pipe connections for cooling and 2 pipes for heating).

The maximum total supply air for the product is limited to 90 ltrs/sec, which equates to 25 ltrs/sec/m for a 3.6m long beam.

## At a glance

- Drop down heat exchange battery for easy cleaning to all four sides of the heat exchanger.
- High output "**1121 W/m**".
- Can accommodate up to 90 ltrs/sec.
- Optimise discharge nozzles sizes and pitch factory set to best suit project requirements.
- Coanda effect is initiated within the beam.
- Discharge veins are concealed within the beam for improved aesthetics.
- **Fan shape distribution for increased occupancy comfort.**
- Unique fast fixing of removable underplates that prevents any sagging even on long beam lengths of 3.6m.
- Various different perforation patterns available for removable underplates.
- Multiple manifold variants to enable reduced chilled (and LTHW, if applicable) water mass flow rates to be facilitated for increased energy efficiencies.
- Operates well at "**Low Pressure**" and "**Low Air Volume**" for increased energy efficiencies.
- Provides indoor climate in accordance with **BS EN ISO 7730**.

# Hygiene

It is important to clean the product to ensure that it looks its best, that it operates at an optimum level, that it will last as long as possible and that it does not present an infection control risk. During development of the Frenger Eco-Healthcare HQ chilled beam the ease of cleaning was of the highest priority.



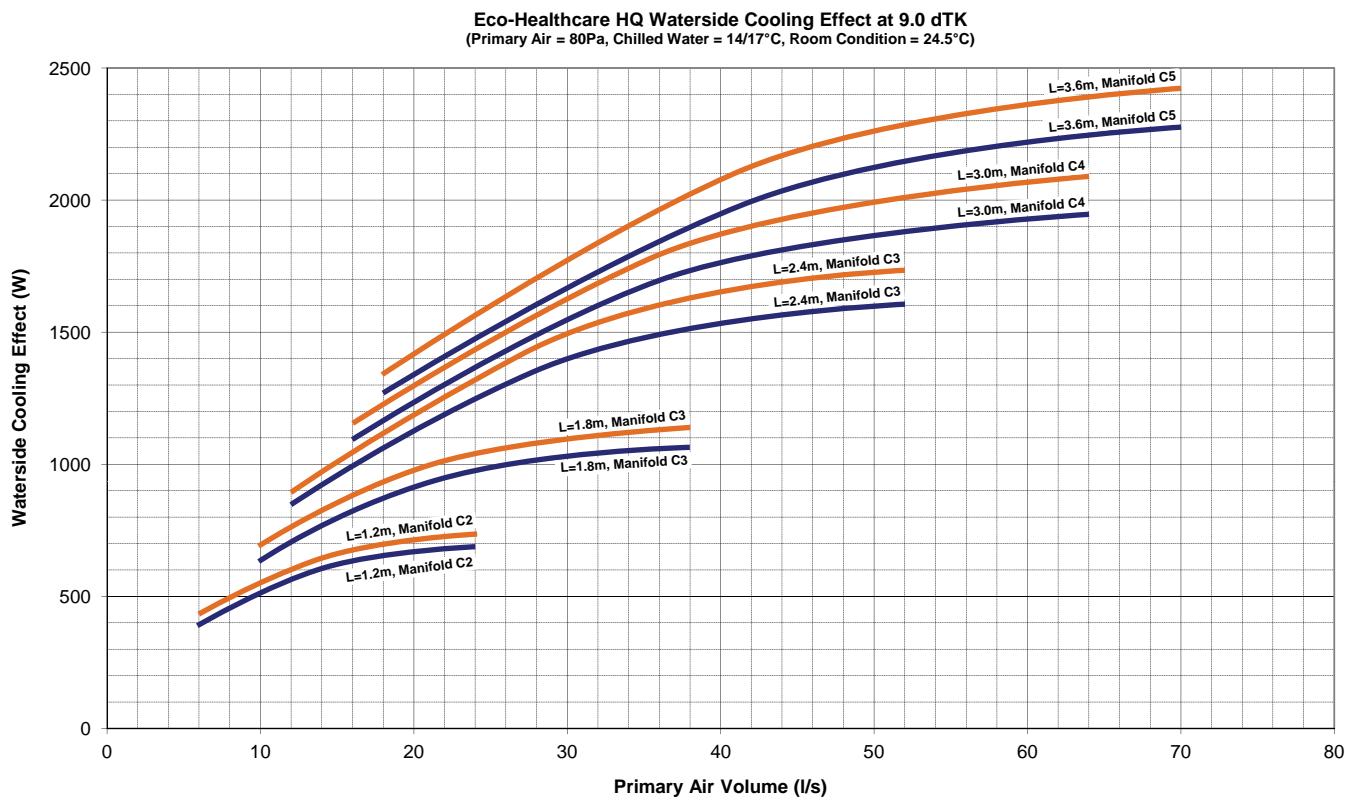
The underplate to the Eco-Healthcare HQ is simple to lower or totally remove. The underplate hooks onto a patent pending extruded aluminium section which is part of the fin coil battery. When "joggled" off the extrusion the underplate can hang on the factory fitted safety cords.



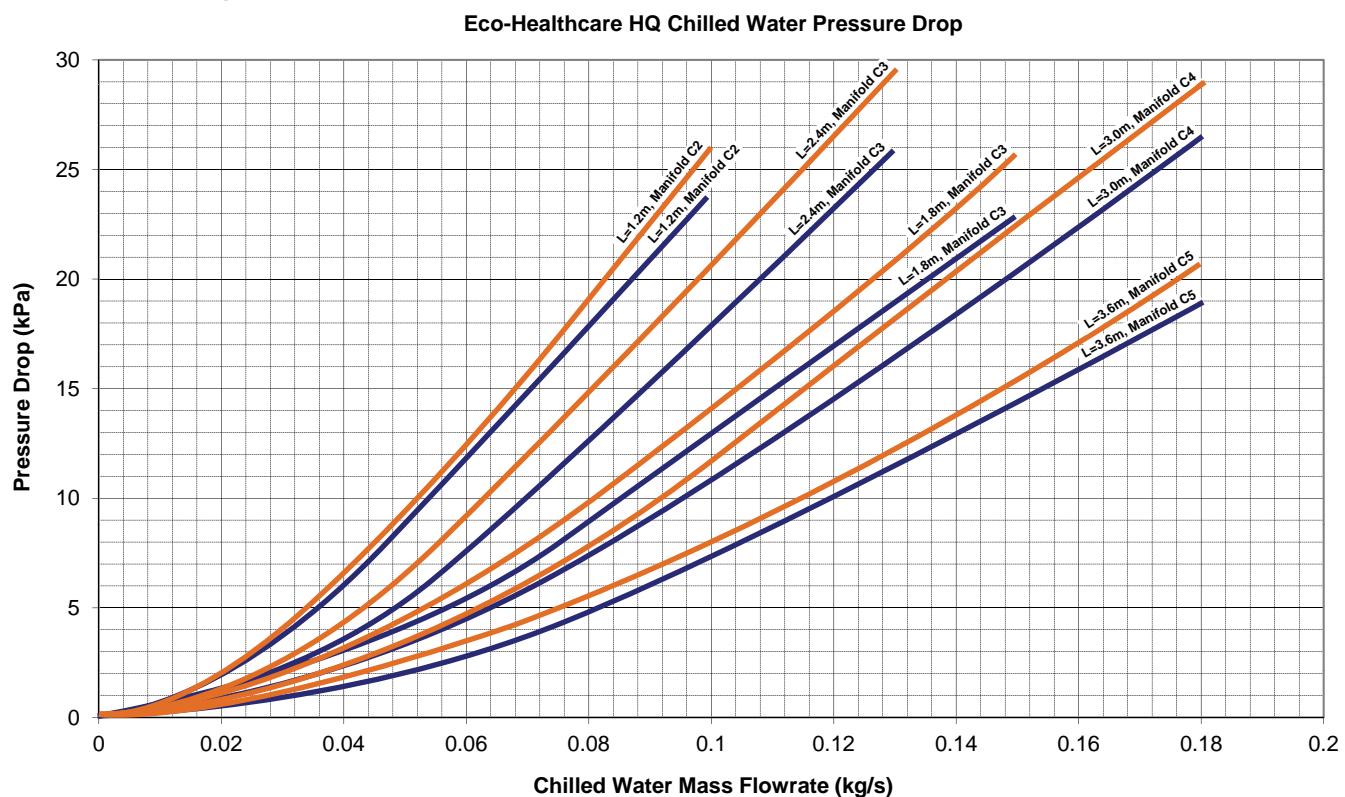
When the underplate is either hanging down on the safety cords or totally removed, the fin coil battery is accessible from below. The fin coil battery can be easily lowered by the removal of four retaining screws (pozi headed screwdriver) to enable 60mm clearance behind the fin coil battery and ample clearance to both sides where air passes.



# Cooling Performance



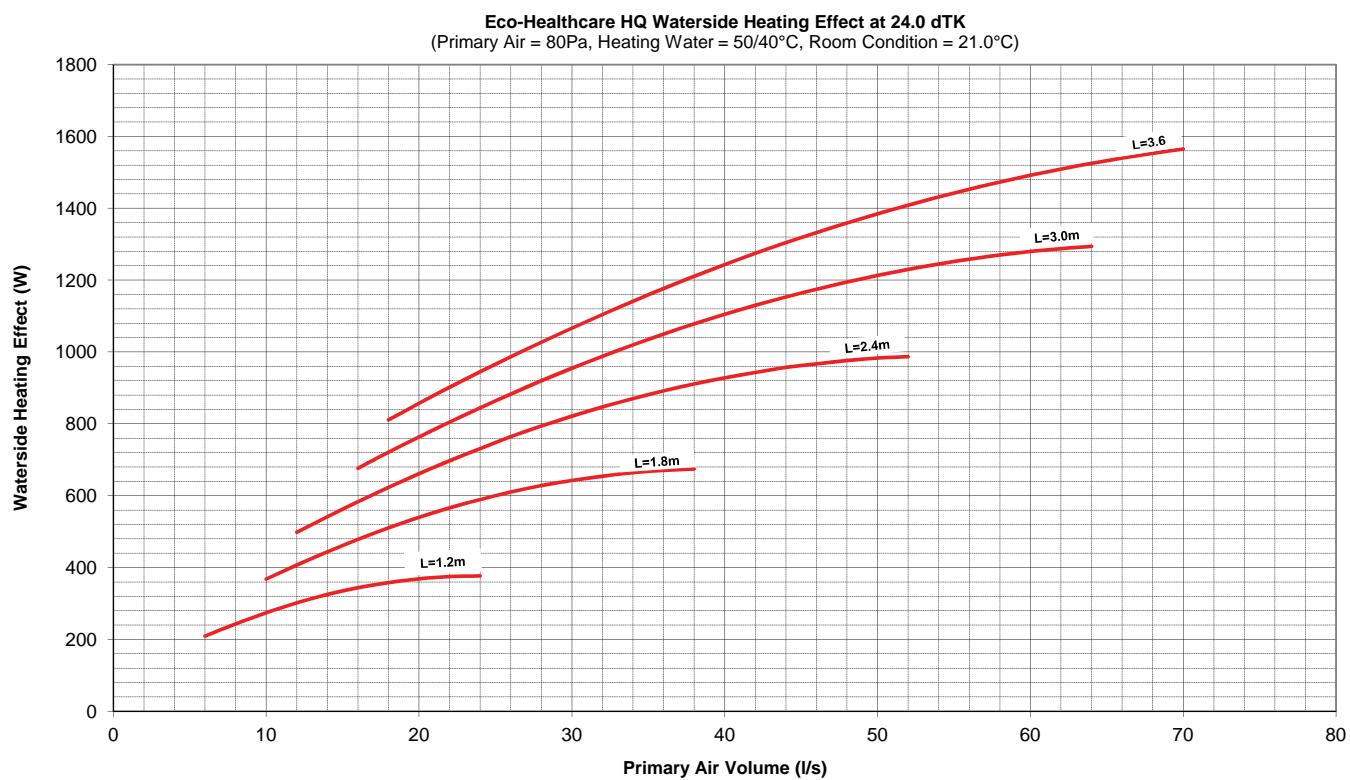
## Pressure Drop



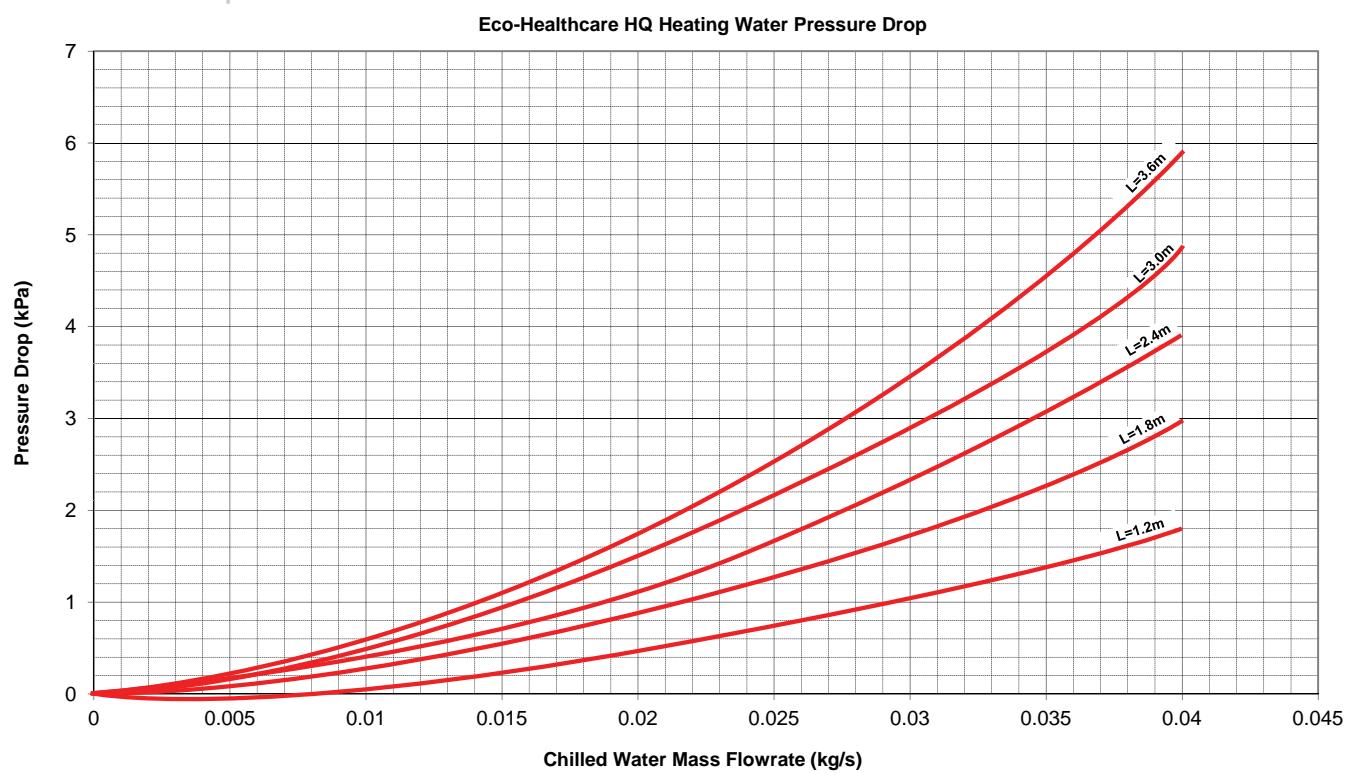
### Legend:

- = Cooling Only
- = Cooling & Heating

# Heating Performance



## Pressure Drop











# Heating Selection Tables

## Heating at 40Pa Nozzle Pressure

Q (l/s)	Nozzle Pressure 40 Pa		Water											
	Eco-H HQ		$\Delta tK - 15^\circ C$			$\Delta tK - 20^\circ C$			$\Delta tK - 25^\circ C$			$\Delta tK - 30^\circ C$		
	L (m)	P (w)	p(kg/s)	p(kPa)										
10	1.2	291	0.012	0.5	358	0.012	0.4	442	0.012	0.5	516	0.012	0.5	
	1.8	349	0.012	0.7	446	0.012	0.8	546	0.013	0.9	675	0.016	1.2	
	2.4	401	0.012	1.0	505	0.012	1.0	652	0.016	1.6	801	0.019	2.3	
	3.0	447	0.012	1.3	581	0.014	1.6	747	0.018	2.5	915	0.022	3.6	
	3.6	-	-	-	-	-	-	-	-	-	-	-	-	
20	1.2	-	-	-	-	-	-	-	-	-	-	-	-	
	1.8	456	0.012	0.8	608	0.015	1.0	797	0.019	1.7	986	0.024	2.4	
	2.4	528	0.013	1.1	746	0.018	2.0	966	0.023	3.2	1187	0.028	4.5	
	3.0	613	0.015	1.8	856	0.020	3.2	1100	0.026	5.0	1343	0.032	7.1	
	3.6	684	0.016	2.6	949	0.023	4.6	1214	0.029	7.1	1477	0.035	10.1	
30	1.2	-	-	-	-	-	-	-	-	-	-	-	-	
	1.8	-	-	-	-	-	-	-	-	-	-	-	-	
	2.4	646	0.015	1.6	912	0.022	2.9	1178	0.028	4.5	1438	0.034	6.3	
	3.0	766	0.018	2.6	1070	0.026	4.7	1369	0.033	7.3	1663	0.040	10.3	
	3.6	862	0.021	3.9	1194	0.029	6.9	1521	0.036	10.6	1843	0.044	14.8	
40	1.2	-	-	-	-	-	-	-	-	-	-	-	-	
	1.8	-	-	-	-	-	-	-	-	-	-	-	-	
	2.4	-	-	-	-	-	-	-	-	-	-	-	-	
	3.0	871	0.021	3.3	1212	0.029	5.9	1544	0.037	9.0	1871	0.045	12.6	
	3.6	1002	0.024	5.1	1380	0.033	8.9	1750	0.042	13.5	-	-	-	

Flow-adjusted waterside heating effect table. Heating circuit  $\Delta t = 10^\circ C$  (Water in-out), nozzle pressure of 40 Pa, 1 x Ø125 air connection.

For red values, the flow rate has been adjusted to the recommended minimum flow of 0.012 kg/s.

## Heating at 60Pa Nozzle Pressure

Q (l/s)	Nozzle Pressure 60 Pa		Water											
	Eco-H HQ		$\Delta tK - 15^\circ C$			$\Delta tK - 20^\circ C$			$\Delta tK - 25^\circ C$			$\Delta tK - 30^\circ C$		
	L (m)	P (w)	p(kg/s)	p(kPa)										
10	1.2	298	0.012	0.4	376	0.012	0.4	445	0.012	0.4	548	0.013	0.6	
	1.8	362	0.012	0.7	452	0.012	0.7	580	0.014	1.0	718	0.017	1.4	
	2.4	428	0.012	1.1	540	0.013	1.1	700	0.017	1.8	862	0.021	2.6	
	3.0	-	-	-	-	-	-	-	-	-	-	-	-	
	3.6	-	-	-	-	-	-	-	-	-	-	-	-	
20	1.2	359	0.012	0.4	448	0.012	0.4	586	0.014	0.6	738	0.018	0.9	
	1.8	465	0.012	0.7	649	0.016	1.2	849	0.020	1.9	1048	0.025	2.7	
	2.4	561	0.013	1.2	791	0.019	2.2	1023	0.025	3.5	1253	0.030	5.0	
	3.0	650	0.016	2.0	908	0.022	3.6	1165	0.028	5.5	1419	0.034	7.8	
	3.6	729	0.017	2.9	1011	0.024	5.2	1290	0.031	7.9	1565	0.037	11.1	
30	1.2	-	-	-	-	-	-	-	-	-	-	-	-	
	1.8	525	0.013	0.8	756	0.018	1.5	990	0.024	2.4	1221	0.029	3.5	
	2.4	692	0.017	1.8	975	0.023	3.2	1255	0.030	5.0	1531	0.037	7.1	
	3.0	814	0.019	2.9	1133	0.027	5.2	1446	0.035	8.0	1755	0.042	11.3	
	3.6	913	0.022	4.3	1261	0.030	7.6	1602	0.038	11.6	1938	0.046	16.2	
40	1.2	-	-	-	-	-	-	-	-	-	-	-	-	
	1.8	-	-	-	-	-	-	-	-	-	-	-	-	
	2.4	765	0.018	2.1	1079	0.026	3.8	1387	0.033	5.9	1688	0.040	8.4	
	3.0	934	0.022	3.7	1296	0.031	6.6	1649	0.040	10.1	1999	0.048	14.2	
	3.6	1064	0.025	5.7	1462	0.035	9.9	1852	0.044	14.9	-	-	-	

Flow-adjusted waterside heating effect table. Heating circuit  $\Delta t = 10^\circ C$  (Water in-out), nozzle pressure of 60 Pa, 1 x Ø125 air connection.

For red values, the flow rate has been adjusted to the recommended minimum flow of 0.012 kg/s.

## Heating at 80Pa Nozzle Pressure

Nozzle Pressure 80 Pa		Water											
Q (l/s)	Eco-H HQ	ΔtK - 15 °C			ΔtK - 20 °C			ΔtK - 25 °C			ΔtK - 30 °C		
	L (m)	P (w)	p(kg/s)	p(kPa)									
10	1.2	316	0.012	0.5	393	0.012	0.5	463	0.012	0.4	580	0.014	0.6
	1.8	379	0.012	0.7	470	0.012	0.7	615	0.015	1.1	763	0.018	1.5
	2.4	-	-	-	-	-	-	-	-	-	-	-	-
	3.0	-	-	-	-	-	-	-	-	-	-	-	-
	3.6	-	-	-	-	-	-	-	-	-	-	-	-
20	1.2	385	0.012	0.4	480	0.012	0.4	642	0.015	0.7	807	0.019	1.1
	1.8	484	0.012	0.7	690	0.017	1.3	901	0.022	2.1	1111	0.027	3.0
	2.4	593	0.014	1.3	836	0.020	2.5	1079	0.026	3.8	1319	0.032	5.4
	3.0	688	0.016	2.2	960	0.023	3.9	1229	0.029	6.1	1493	0.036	8.5
	3.6	774	0.019	3.2	1072	0.026	5.7	1365	0.033	8.8	1651	0.040	12.2
30	1.2	-	-	-	-	-	-	-	-	-	-	-	-
	1.8	573	0.014	0.9	825	0.020	1.8	1079	0.026	2.8	1330	0.032	4.1
	2.4	738	0.018	2.0	1037	0.025	3.6	1334	0.032	5.5	1625	0.039	7.8
	3.0	861	0.021	3.2	1195	0.029	5.8	1523	0.036	8.8	1847	0.044	12.3
	3.6	965	0.023	4.8	1327	0.032	8.3	1682	0.040	12.6	2034	0.049	17.6
40	1.2	-	-	-	-	-	-	-	-	-	-	-	-
	1.8	-	-	-	-	-	-	-	-	-	-	-	-
	2.4	833	0.020	2.4	1174	0.028	4.4	1507	0.036	6.9	1833	0.044	9.7
	3.0	998	0.024	4.2	1381	0.033	7.4	1756	0.042	11.3	-	-	-
	3.6	1126	0.027	6.3	1544	0.037	10.9	1957	0.047	16.5	-	-	-

Flow-adjusted waterside heating effect table. Heating circuit  $\Delta t = 10^\circ\text{C}$  (Water in-out), nozzle pressure of 80 Pa, 1 x Ø125 air connection.

For red values, the flow rate has been adjusted to the recommended minimum flow of 0.012 kg/s.

## Heating at 100Pa Nozzle Pressure

Nozzle Pressure 100 Pa		Water											
Q (l/s)	Eco-H HQ	ΔtK - 15 °C			ΔtK - 20 °C			ΔtK - 25 °C			ΔtK - 30 °C		
	L (m)	P (w)	p(kg/s)	p(kPa)									
10	1.2	322	0.012	0.5	399	0.012	0.5	473	0.012	0.4	591	0.014	0.6
	1.8	386	0.012	0.7	480	0.012	0.7	629	0.015	1.1	781	0.019	1.6
	2.4	-	-	-	-	-	-	-	-	-	-	-	-
	3.0	-	-	-	-	-	-	-	-	-	-	-	-
	3.6	-	-	-	-	-	-	-	-	-	-	-	-
20	1.2	400	0.012	0.5	507	0.012	0.5	673	0.016	0.8	842	0.020	1.2
	1.8	496	0.012	0.7	705	0.017	1.3	918	0.022	2.1	1130	0.027	3.1
	2.4	605	0.014	1.4	852	0.020	2.5	1099	0.026	4.0	1343	0.032	5.6
	3.0	702	0.017	2.3	981	0.023	4.1	1257	0.030	6.3	1528	0.037	8.9
	3.6	793	0.019	3.4	1101	0.026	6.0	1403	0.034	9.2	1700	0.041	12.9
30	1.2	-	-	-	-	-	-	-	-	-	-	-	-
	1.8	602	0.014	1.0	859	0.021	1.9	1117	0.027	3.0	1371	0.033	4.3
	2.4	756	0.018	2.1	1059	0.025	3.7	1357	0.033	5.7	1651	0.040	8.1
	3.0	877	0.021	3.3	1215	0.029	5.9	1547	0.037	9.1	1875	0.045	12.7
	3.6	982	0.024	4.9	1351	0.032	8.6	1713	0.041	13.0	-	-	-
40	1.2	-	-	-	-	-	-	-	-	-	-	-	-
	1.8	652	0.016	1.2	941	0.023	2.2	1228	0.029	3.6	1509	0.036	5.1
	2.4	866	0.021	2.6	1212	0.029	4.7	1550	0.037	7.2	1881	0.045	10.1
	3.0	1020	0.024	4.4	1406	0.034	7.7	1785	0.043	11.6	-	-	-
	3.6	1146	0.027	6.4	1567	0.038	11.2	1983	0.048	16.8	-	-	-

Flow-adjusted waterside heating effect table. Heating circuit  $\Delta t = 10^\circ\text{C}$  (Water in-out), nozzle pressure of 100 Pa, 1 x Ø125 air connection.

For red values, the flow rate has been adjusted to the recommended minimum flow of 0.012 kg/s.

# Air Cooling Effect

Cooling effect supplied in the ventilation air [W]

1. Start by calculating the required cooling effect that has to be supplied to the room in order to provide a certain temperature.
2. Calculate any cooling effect that is provided by the ventilation.
3. The remaining cooling effect has to be supplied by the beam.

Formula for air cooling effect:  $P = m \cdot C_p \cdot \Delta t$

Where:

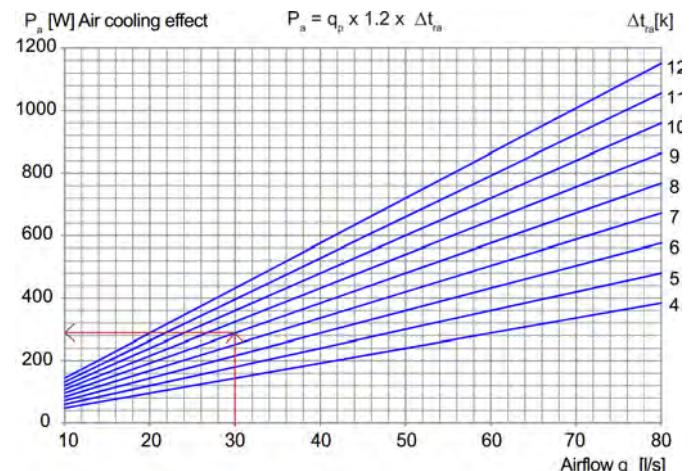
$m$  = mass

$C_p$  = specific heat capacity [J/(kg-K)]

$q_p$  = air flow [l/s]

$\Delta t$  = the difference between the temperature of the room and the temperature of the supply air [K].

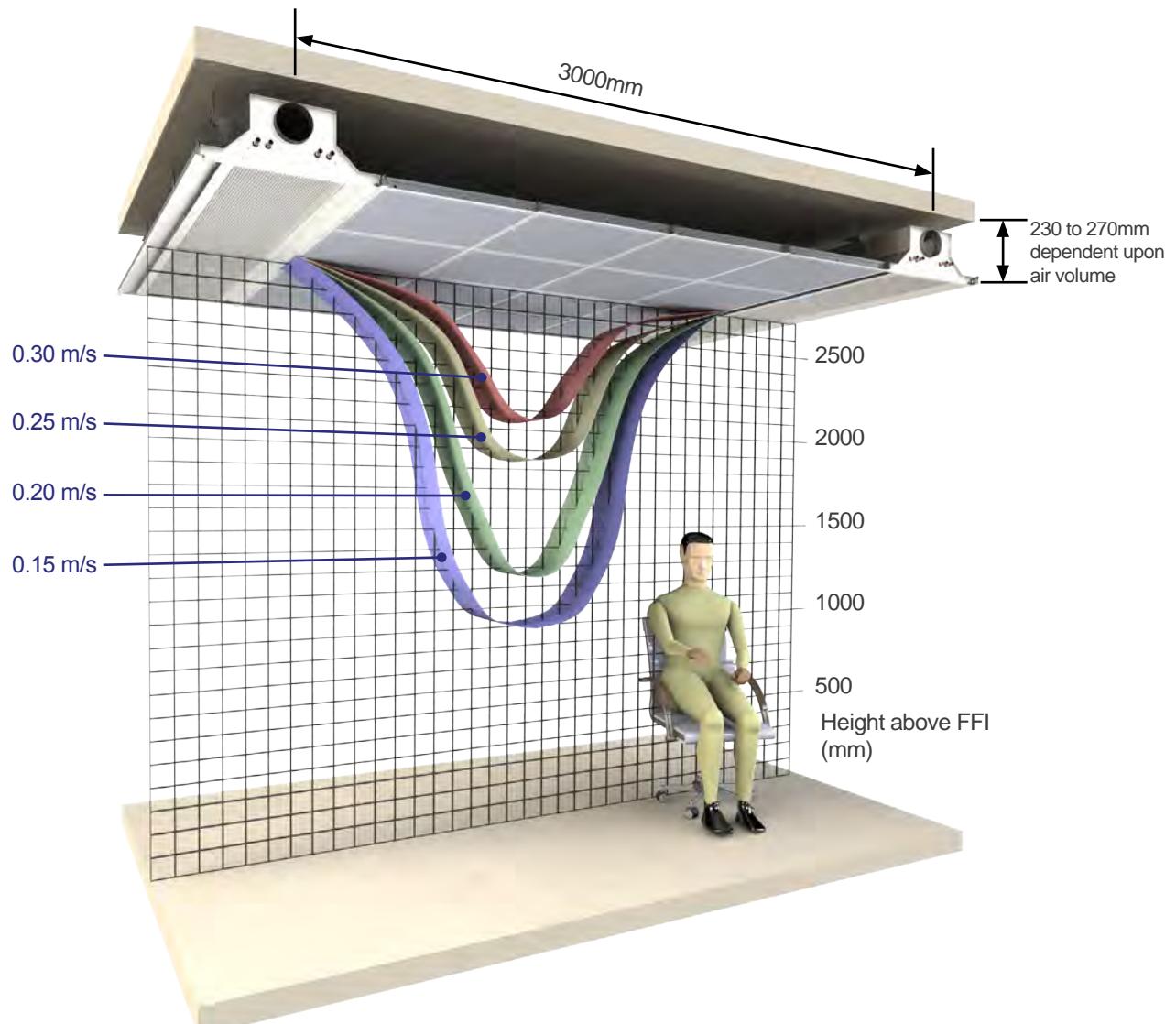
It is usually  $m \cdot C_p \approx q_p \cdot 1.2$



Air cooling effect as a function of airflow. For example, if the air flow is 30 l/s and the under-temperature of the supply air is  $\Delta t_{ra} = 8$ K, the cooling effect from the graph is 290W.

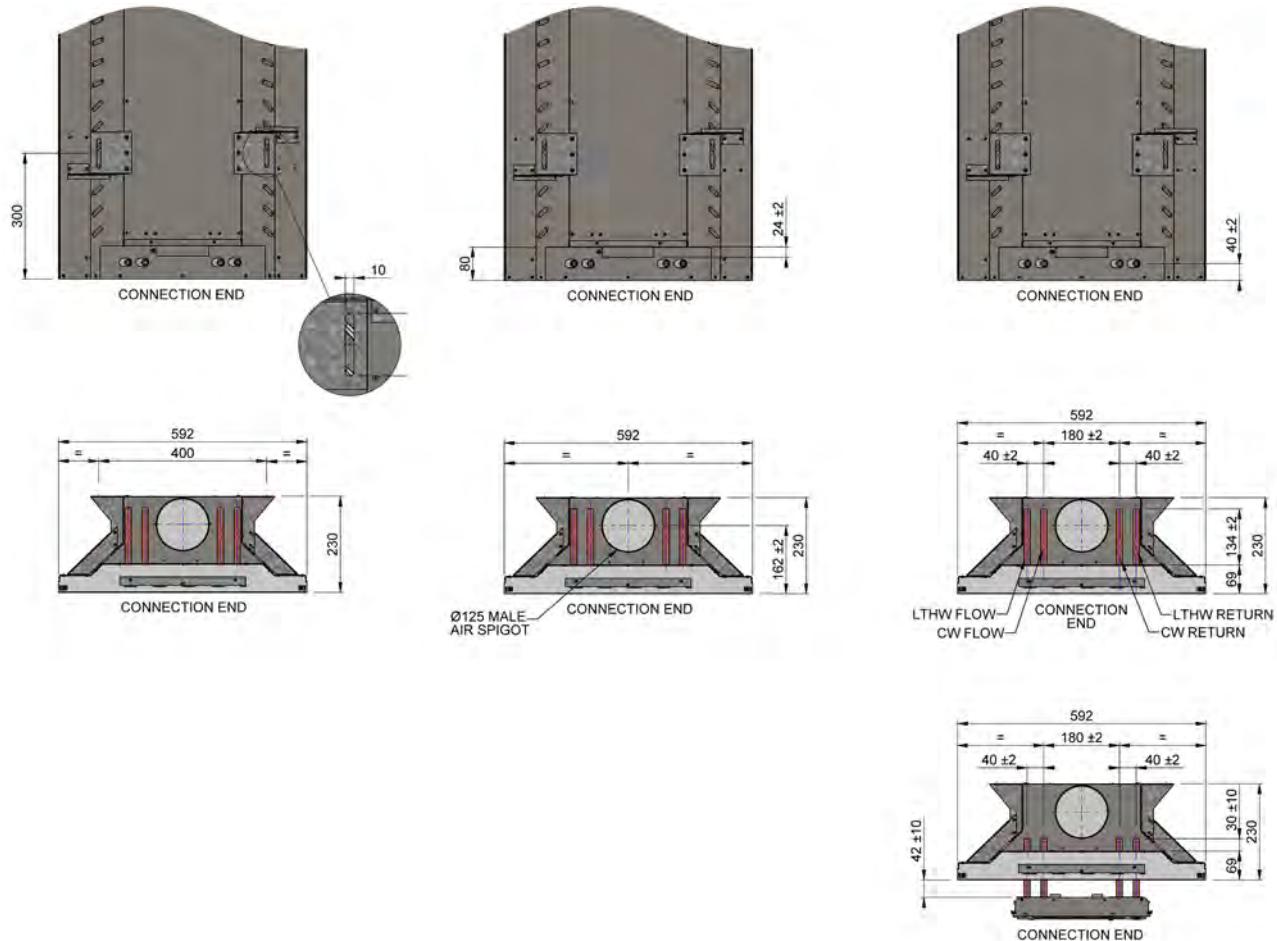
## Scatter Diagram

Fresh Air Volume 22 l / s / Active m @ 80 Pa



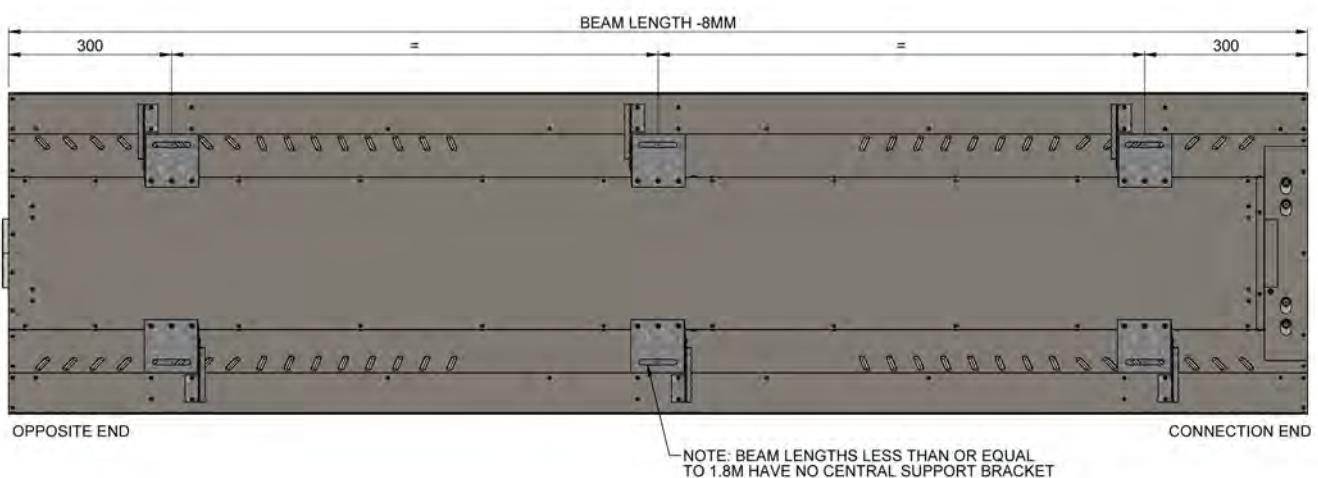
# Product Dimensions

## Eco-Healthcare HQ 125

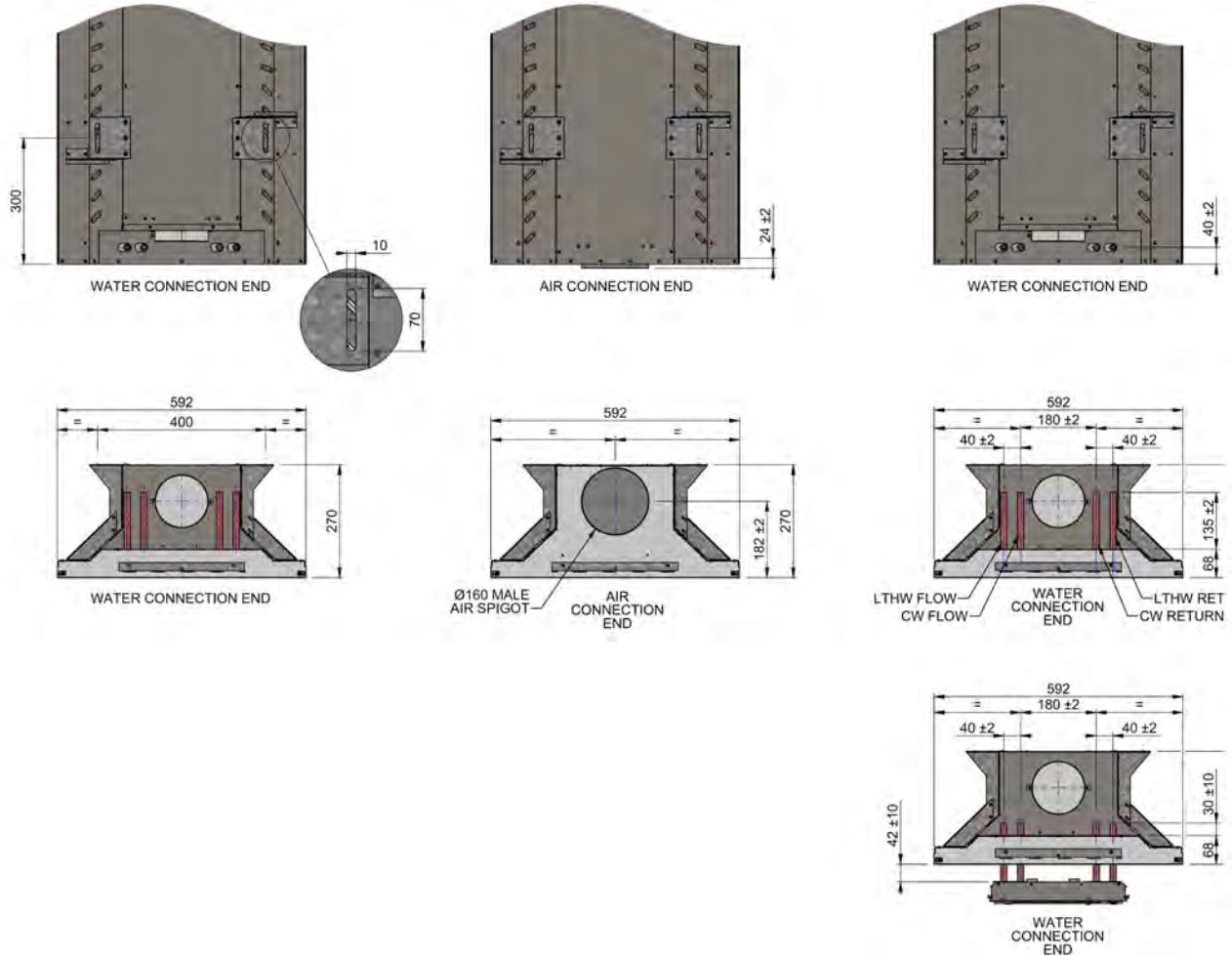


## Mounting Details

### Eco-Healthcare HQ 125

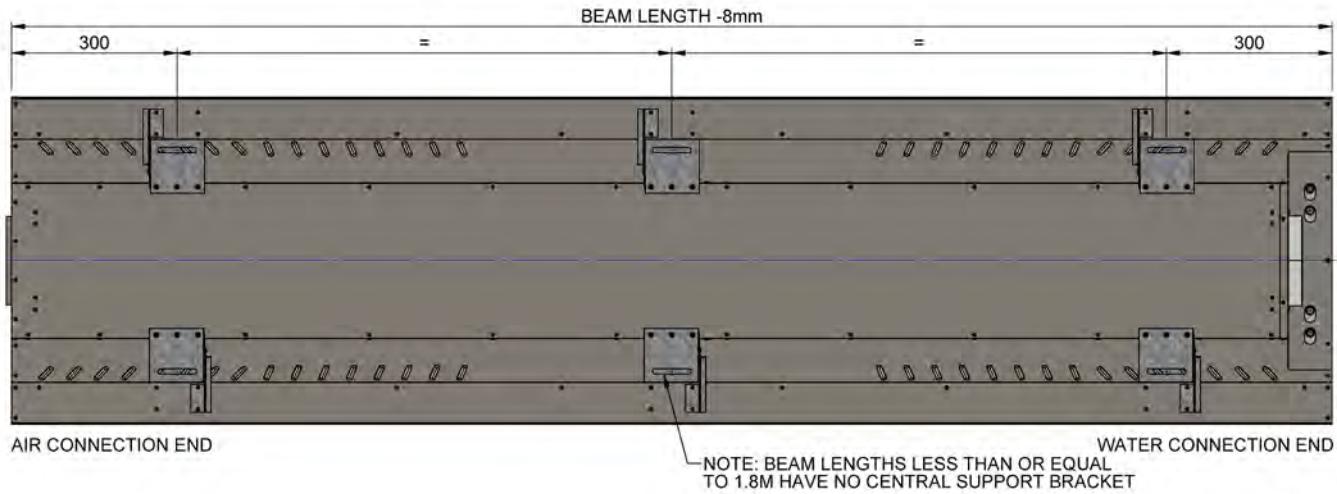


## Eco-Healthcare HQ 125



## Mounting Details

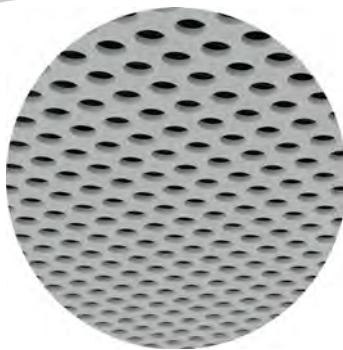
### Eco-Healthcare HQ 125



# Perforation Pattern Options



Slot Perforation  
45% Free Area

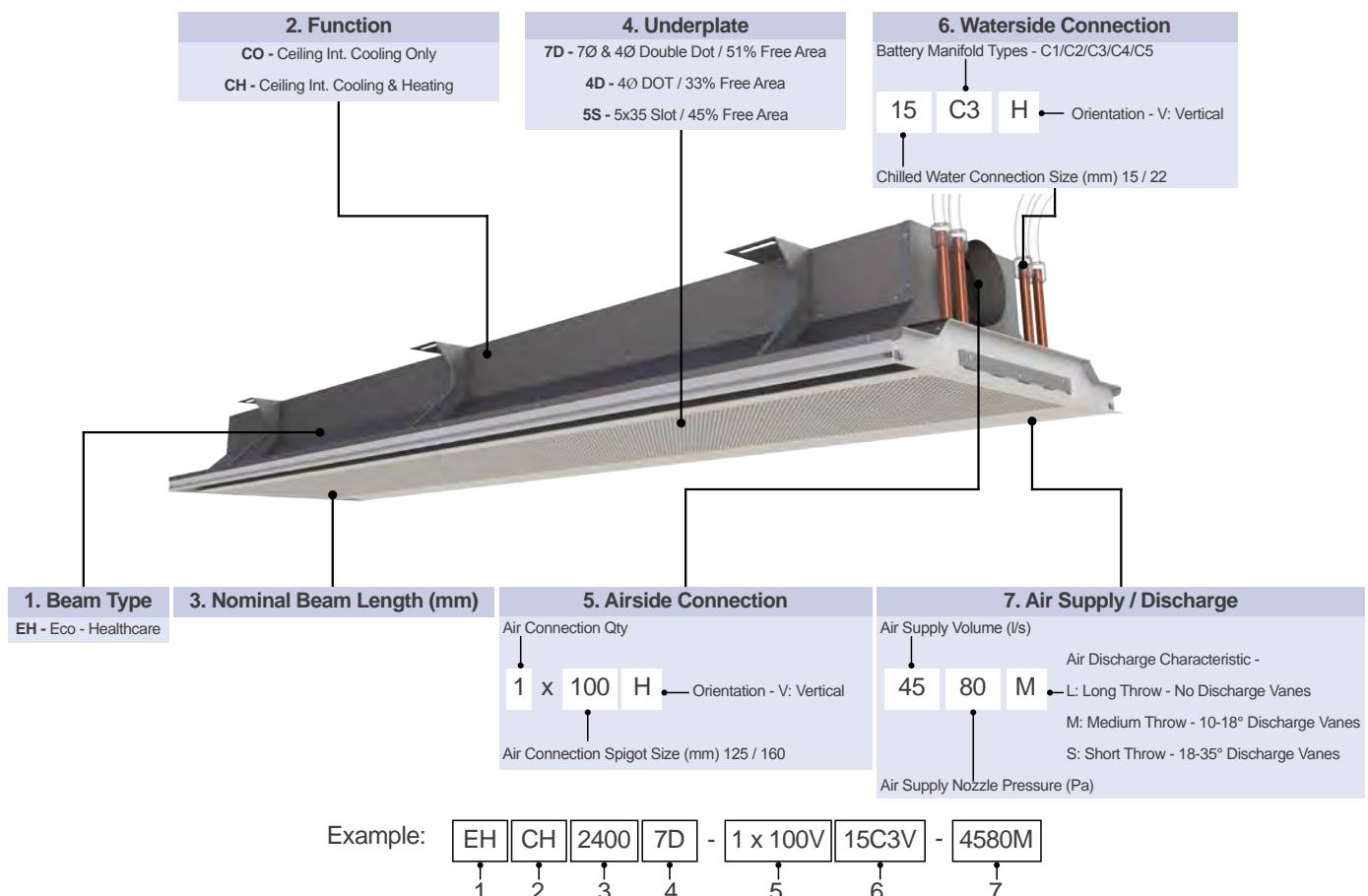


Dot Perforation  
33% Free Area



Double Dot Perforation  
51% Free Area

## Product Ordering Codes



# Calculation Program



## Eco Active Beam Data

Beam Variant	Healthcare
Air Connection	1x125 mm
Product Overall Length	2.4 m
Manifold Type	C4
Air Discharge Throw	S
Nozzle Static Pressure	80 Pa
Fresh Air Supply Volume	25 l/s
Heating Function	H4
Underplate Perforation Type	51% OBR

Frenger's calculation programme for Eco-Healthcare HQ is extremely user friendly.

Simply select from the drop down menu the "Air Connection" configuration. Air volumes in excess of 40 ltrs/sec and up to 50 ltrs/sec should be 2 x 80 diameter.

"Manifold Types" can be changed in the drop down menu for increased waterside cooling effect, however attention needs to be taken regarding resultant pressure drops (hydraulic resistance), If pressure drops need reducing, choose a higher numbered manifold (C5 being the highest and C2 being the lowest).

"Discharge Throw" can be S (short), M (medium) or L (long).

"Underplate Perforated" options can be found on page 14.

Design Conditions	Cooling	Heating
Flow Water Temperature	14.0 °C	45.0 °C
Return Water Temperature	17.0 °C	35.0 °C
Air Supply Temperature	16.0 °C	16.0 °C
Average Room Condition	25.5 °C	16.0 °C
"Air On" Thermal Gradient	1.0 °C	
Room Relative Humidity	45.0 %	

Complete your project data in the "Design Conditions" section. Please note that the "Air On" Thermal Gradient should not be used in normal instances.

Performance Data	Cooling	Heating
Room - Mean Water dT	10.00 K	24.00 K
Air On Coil - Mean Water dT	11.00 K	21.10 K
Waterside Performance	1201 W	1011 W
Water Mass Flowrate	0.096 kg/s	0.024 kg/s
Waterside Pressure Drop	7.2 kPa	3.4 kPa
Airsides Performance	285 W	0 W
Total Sensible Performance	1486 W	1011 W
Sound Effect LW	< 35 dB(A)	

"Performance Data" will then automatically be calculated. Likewise "Dimensional Date" will be also automatically calculated.

Finally, the "Design Check" should read "OK" in green, or detail some warning in red.

Calculation programs for Eco-Healthcare HQ are available upon request.

Contact our technical department or complete an application request form from [www.frenger.co.uk](http://www.frenger.co.uk) from the relevant link on our home page.

Active Chilled Beam Calculation Tool  
[Is this the latest version?](#)

Project Ref.

**Eco HQ Active Beam Data**

Beam Variant	Healthcare
Air Connection	1x125 mm
Product Overall Length	2.4 m
Manifold Type	C4
Air Discharge Throw	S
Nozzle Static Pressure	80 Pa
Fresh Air Supply Volume	25 l/s
Heating Function	H4
Underplate Perforation Type	51% DOT

**FRENGER® systems**  
version 1.3.3

**Design Conditions**

	Cooling	Heating
Flow Water Temperature	14.0 °C	45.0 °C
Return Water Temperature	17.0 °C	35.0 °C
Air Supply Temperature	16.0 °C	16.0 °C
Average Room Condition	25.5 °C	16.0 °C
"Air On" Thermal Gradient	1.0 °C	
Room Relative Humidity	45.0 %	

**Dimensional Data**

Width x Depth	592 x 230 mm
Overall Length	2392 mm
Water Volume	3 l
Dry Weight	46 kg
CW Connection	Ø15 mm
LTHW Connection	Ø15 mm

**Performance Data**

	Cooling	Heating
Room - Mean Water dT	10.00 K	24.00 K
Air On Coil - Mean Water dT	11.00 K	21.10 K
Waterside Performance	1201 W	1011 W
Water Mass Flowrate	0.096 kg/s	0.024 kg/s
Waterside Pressure Drop	7.2 kPa	3.4 kPa
Airsides Performance	285 W	0 W
Total Sensible Performance	1486 W	1011 W
Sound Effect LW	< 35 dB(A)	

Model Ref: EHHQCH24007D-125H15C4H4-2580S

Notes:

1) Performance calculations are based upon normal clean potable water; it is the system engineer's responsibility to allow for any reduction in cooling or heating performance due to additives that may reduce the water systems heat transfer coefficient.

2) Pressure drop calculations are based upon CIBSE guides using clean potable water and exclude any additional losses associated with entry / exit losses, pipe fouling or changes in water quality; it is the system engineer's responsibility to use good engineering practice.

# Project Specific Testing Facility

The 3 number state-of-the-art Climatic Testing Laboratories at Frenger's Derby based technical centre, have internal dimensions of 6.3 x 5.7 x 3.3m high and includes a thermal wall so that both core and perimeter zones can be modelled. The test facilities are fixed in overall size and construction therefore simulation of a buildings specific thermall mass cannot be completed, it should, however be noted that a specific project can be simulated more accurately by recessing the floor and reducing the height as necessary.

## Project Specific Testing

Project specific mock-up testing is a valuable tool which allows the Client to fully asses the proposed system and determine the resulting indoor quality and comfort conditions; the physical modeling is achieved by installing a full scale representation of a building zone complete with internal & external heat gains (Lighting, Small Power, Occupancy & Solar Gains).

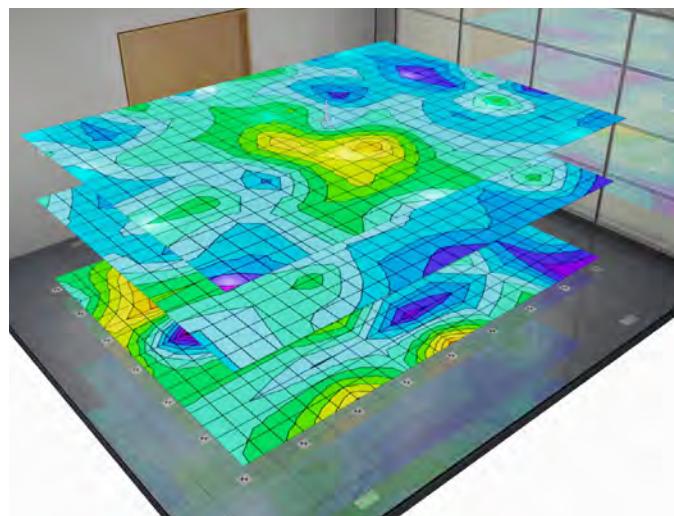
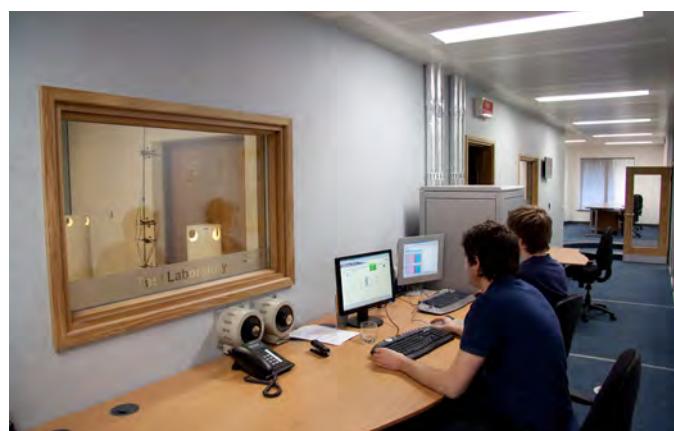
The installed mock-up enables the client to verify the following:

- Product performance under project specific conditions.
- Spatial air temperature distribution.
- Spatial air velocities.
- Experience thermal comfort.
- Project specific aesthetics.
- Experience lighting levels (where relevant).
- Investigate the specific design and allow the system to be enhanced.



The project-specific installation and test is noramlly conducted to verify:

- Product capacity under design conditions.
- Comfort levels -air temperature distribution  
-thermal stratification  
-draft risk  
-radiant temperature analysis
- Smoke test video illustrating air movement.



# Photometric Testing Facility

The photometric test laboratories at Frenger Systems are used to evaluate the performance of luminaires. To measure the performance, it is necessary to obtain values of light intensity distribution from the luminaire. These light intensity distributions are used to mathematically model the lighting distribution envelope of a particular luminaire. This distribution along with the luminaire's efficacy allows for the generation of a digital distribution that is the basis of the usual industry standard electronic file format. In order to assess the efficacy of the luminaire it is a requirement to compare the performance of the luminaire against either a calibrated light source for absolute output or against the "bare" light source for a relative performance ratio.

The industry uses both methods. Generally absolute lumen outputs are used for solid state lighting sources and relative lighting output ratios (LOR) are used for the more traditional sources. Where the LOR method is chosen then published lamp manufacturer's data is used to calculate actual lighting levels in a scheme.

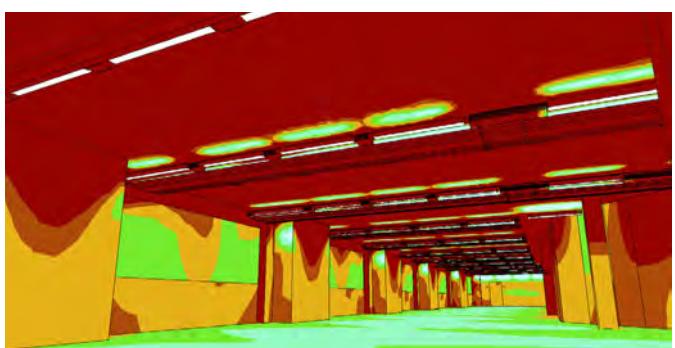
The intensity distribution is obtained by the use of a Goniophotometer to measure the intensity of light emitted from the surface of the fitting at pre-determined angles. The light intensity is measured using either a photometer with a corrective spectral response filter to match the CIE standard observer curves or our spectrometer for LED sources.

Luminaire outputs are measured using our integrating sphere from small luminaires or our large integrator room for large fittings and Multi Service Chilled Beams. For both methods we can use traceable calibrated radiant flux standards for absolute comparisons.

All tests use appropriate equipment to measure and control the characteristics of the luminaire and include air temperature measurements, luminaire supply voltage, luminaire current and power. Thermal characteristics of luminaire components can be recorded during the testing process as required.

A full test report is compiled and supplied in "locked" PDF format. Data is collected and correlated using applicable software and is presented electronically to suit, usually in Eulumdat, CIBSE TM14 or IESN standard file format.

Frenger conduct photometric test in accordance with CIE 127:2007 and BS EN 13032-1 and sound engineering practice as applicable. During the course of these tests suitable temperature measurements of parts of LED's can be recorded. These recorded and plotted temperature distributions can be used to provide feedback and help optimise the light output of solid state light source based on luminaires which are often found to be sensitive to junction temperatures.



# Acoustic Testing Facility

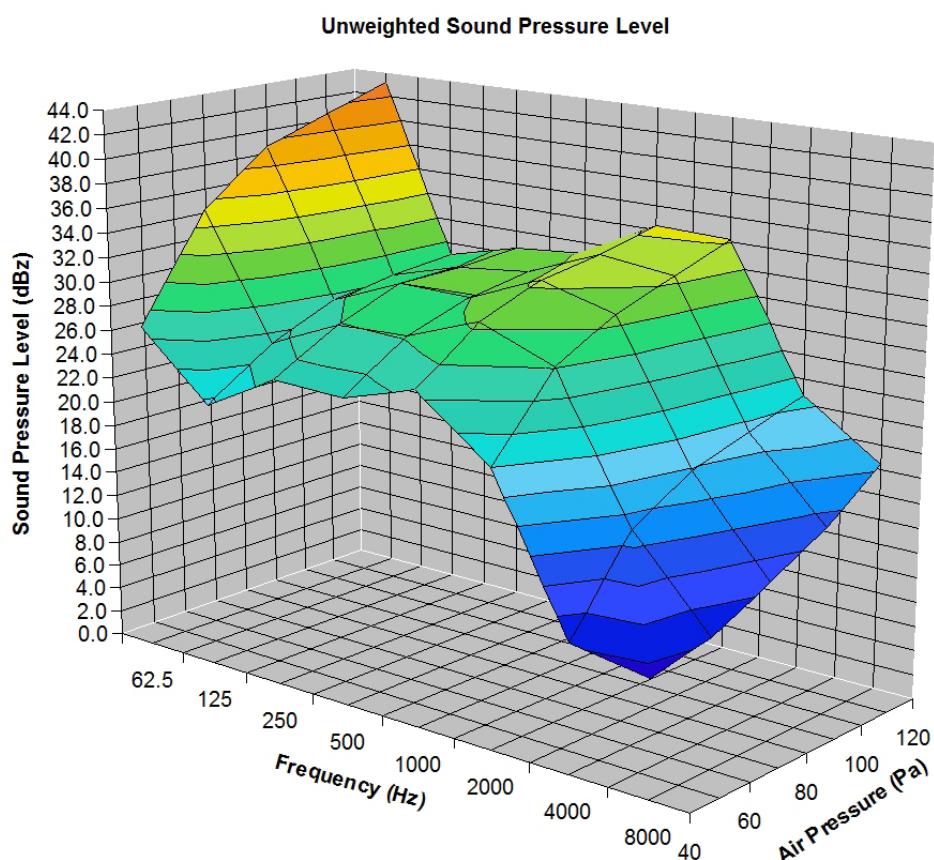
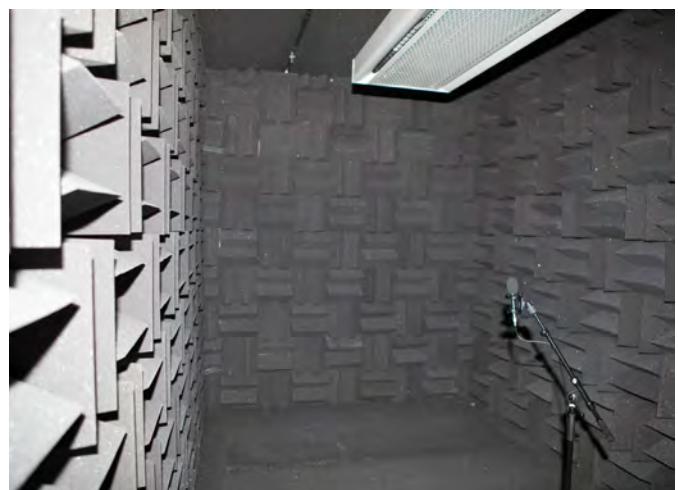
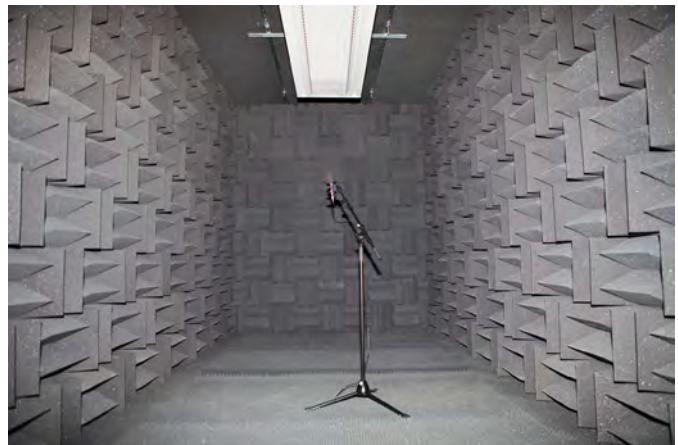
The Acoustic Test Room at Frenger is a hemi-anechoic chamber which utilises sound absorbing acoustic foam material in the shape of wedges to provide an echo free zone for acoustic measurements; the height of the acoustic foam wedges has a direct relationship with the maximum absorption frequency, hence Frenger has the wedges specifically designed to optimise the sound absorption at the peak frequency normally found with our active chilled beam products.

The use of acoustic absorbing material within the test room provides the simulation of a quiet open space without "reflections" which helps to ensure sound measurements from the sound source are accurate, in addition the acoustic material also helps reduce external noise entering the test room meaning that relatively low levels of sound can be accurately measured.

The acoustic facilities allow Frenger to provide express in-house sound evaluation so that all products, even project specific designs can be assessed and optimised.

To ensure accuracy Frenger only uses Class 1 measurement equipment which allows sound level measurements to be taken at 11 different  $\frac{1}{3}$  octave bands between 16 Hz to 16 kHz, with A, C and Z (un-weighted) simultaneous weightings.

In addition to the above, Frenger also send their new products for specialist third party Acoustic Testing. The results of which are very close and within measurement tolerances to that of Frenger's in-house measurement of sound.







Frenger Systems participates in the ECC programme for Chilled Beams.  
Check ongoing validity of certificate:  
[www.eurovent-certification.com](http://www.eurovent-certification.com) or  
[www.certiflash.com](http://www.certiflash.com)

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